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PROPAGATION OF RAYLEIGH-TYPE WAVES
IN AEOLOTROPIC MATERIAL WITH CUBIC SYMMETRY

SUBHAS DUTTA and PRIYATOSH ROY

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INTRODUCTION

Miller and Musgrave studied the propagation of elastic waves in cubic materials. In this paper we have studied the possibility of propagation of Rayleigh-type waves in aeolotropic material with cubic symmetry. Three different models have been considered: (i) a semi-infinite medium of the material, (ii) a layer of the material, of finite thickness, resting on a rigid base, and (iii) a semi-infinite isotropic medium overlaid by a layer of finite thickness of the material. For numerical calculation, the values of the elastic constants are taken to be those for pyrites [Love — p. 163].

SOLUTION OF THE PROBLEM

(A) With the origin at the free surface and the axes of symmetry as the axes of reference, Z-axis being directed into the medium, the equations of motion for cubic material in two dimensions are

$$(1) \quad c_{11} \frac{\partial^2 u}{\partial x^2} + c_{44} \frac{\partial^2 u}{\partial z^2} + (c_{12} + c_{44}) \frac{\partial^2 \omega}{\partial x \partial z} = \rho \frac{\partial^2 u}{\partial t^2}$$

and

$$(2) \quad c_{44} \frac{\partial^2 \omega}{\partial x^2} + c_{11} \frac{\partial^2 \omega}{\partial z^2} + (c_{12} + c_{44}) \frac{\partial^2 u}{\partial x \partial z} = \rho \frac{\partial^2 \omega}{\partial t^2},$$

where u and w are the components of displacement in the x and z directions, respectively.

Substituting

$$(3) \quad u = \frac{\partial \varphi}{\partial x} + \frac{\partial^2 \psi}{\partial x \partial z},$$

$$\omega = \frac{\partial \varphi}{\partial z} + \frac{\partial^2 \psi}{\partial z^2} + \alpha \psi$$

in equations (1) and (2), α being a constant to be chosen suitably, we get

$$(4) \quad \frac{\partial}{\partial x} \left[c_{11} \frac{\partial^2 \varphi}{\partial x^2} + (c_{12} + 2c_{44}) \frac{\partial^2 \varphi}{\partial z^2} - \varrho \frac{\partial^2 \varphi}{\partial t^2} + \right. \\ \left. + \frac{\partial}{\partial z} \left\{ c_{11} \frac{\partial^2 \psi}{\partial x^2} + (c_{12} + 2c_{44}) \frac{\partial^2 \psi}{\partial z^2} + (c_{12} + c_{44}) \alpha \psi - \varrho \frac{\partial^2 \psi}{\partial t^2} \right\} \right] = 0$$

and

$$(5) \quad \frac{\partial}{\partial z} \left[c_{11} \frac{\partial^2 \varphi}{\partial z^2} + (c_{12} + 2c_{44}) \frac{\partial^2 \varphi}{\partial x^2} - \varrho \frac{\partial^2 \varphi}{\partial t^2} \right] + \\ + \frac{\partial^2}{\partial z^2} \left[c_{11} \frac{\partial^2 \psi}{\partial z^2} + (c_{12} + 2c_{44}) \frac{\partial^2 \psi}{\partial x^2} - \varrho \frac{\partial^2 \psi}{\partial t^2} \right] + \\ + \alpha \left[c_{44} \frac{\partial^2 \psi}{\partial x^2} + c_{11} \frac{\partial^2 \psi}{\partial z^2} - \varrho \frac{\partial^2 \psi}{\partial t^2} \right] = 0.$$

Now let us assume

$$(6) \quad \varphi = A \cos kx e^{-qz} e^{ipt} \\ \psi = B \cos kx e^{-qz} e^{ipt}.$$

Then equations (4) and (5) are satisfied if

$$(7) \quad A[(c_{12} + 2c_{44})q^2 + (\varrho p^2 - c_{11}k^2)] - Bq[(c_{12} + 2c_{44})q^2 + \\ + \{(c_{12} + c_{44})\alpha + \varrho p^2 - c_{11}k^2\}] = 0$$

and

$$(8) \quad Aq[c_{11}q^2 + \{\varrho p^2 - k^2(c_{12} + 2c_{44})\}] - \\ - B[q^2\{c_{11}q^2 + \varrho p^2 - k^2(c_{12} + 2c_{44})\} + \alpha\{c_{11}q^2 + \varrho p^2 - c_{44}k^2\}] = 0.$$

Eliminating A and B from (7) and (8) we see that in order that (6) may satisfy equations (4) and (5), q must satisfy

$$(9) \quad c_{11}c_{44}q^4 + [(c_{44} + c_{11})\varrho p^2 + (c_{12}^2 - c_{11}^2 + 2c_{12}c_{44})k^2]q^2 + \\ + (\varrho p^2 - c_{11}k^2)(\varrho p^2 - c_{44}k^2) = 0.$$

If $\pm q_1$ and $\pm q_2$ are the roots of equation (9) we may write

$$(10) \quad \varphi = (A_1 e^{q_1 z} + A_2 e^{-q_1 z} + A_3 e^{q_2 z} + A_4 e^{-q_2 z}) \cos kx e^{ipt}, \\ \psi = (B_1 e^{q_1 z} + B_2 e^{-q_1 z} + B_3 e^{q_2 z} + B_4 e^{-q_2 z}) \cos kx e^{ipt},$$

where

$$(11) \quad \begin{aligned} q_1 B_1 &= \xi A_1, \\ q_1 B_2 &= -\xi A_2, \\ q_2 B_3 &= \eta A_3, \\ q_2 B_4 &= -\eta A_4, \end{aligned}$$

ξ and η being given by

$$(12) \quad \begin{aligned} \xi &= \frac{(c_{12} + 2c_{44}) q_1^2 + \varrho p^2 - c_{11} k^2}{(c_{12} + 2c_{44}) q_1^2 + \varrho p^2 - c_{11} k^2 + (c_{12} + c_{44}) \alpha}, \\ \eta &= \frac{(c_{12} + 2c_{44}) q_2^2 + \varrho p^2 - c_{11} k^2}{(c_{12} + 2c_{44}) q_2^2 + \varrho p^2 - c_{11} k^2 + (c_{12} + c_{44}) \alpha}. \end{aligned}$$

From (3), (10) and (11) we get

$$(13) \quad u = -k \sin kx e^{ipt} [(1 + \xi) A_1 e^{q_1 z} + (1 + \xi) A_2 e^{-q_1 z} + (1 + \eta) A_3 e^{q_2 z} + (1 + \eta) A_4 e^{-q_2 z}],$$

$$(14) \quad \omega = \cos kx e^{ipt} \left[\left\{ q_1 + \left(\frac{q_1^2 + \alpha}{q_1} \right) \xi \right\} A_1 e^{q_1 z} - \left\{ q_1 + \left(\frac{q_1^2 + \alpha}{q_1} \right) \xi \right\} A_2 e^{-q_1 z} + \left\{ q_2 + \left(\frac{q_2^2 + \alpha}{q_2} \right) \eta \right\} A_3 e^{q_2 z} - \left\{ q_2 + \left(\frac{q_2^2 + \alpha}{q_2} \right) \eta \right\} A_4 e^{-q_2 z} \right].$$

(B) If, however, instead of (3), we substitute

$$(15) \quad \begin{aligned} u &= \frac{\partial \varphi}{\partial x} + \frac{\partial^2 \psi}{\partial x \partial z}, \\ \omega &= \frac{\partial \varphi}{\partial z} + \frac{\partial^2 \psi}{\partial z^2} \end{aligned}$$

in equations (1) and (2) and assume the same form of solutions for φ and ψ as in (6), we find that the values of $\pm q_1$ and $\pm q_2$ are given by

$$(16) \quad \begin{aligned} q_1^2 &= \frac{(c_{11} - \varrho c^2) k^2}{c_{12} + 2c_{44}}, \\ q_2^2 &= \frac{(c_{12} + 2c_{44} - \varrho c^2) k^2}{c_{11}}. \end{aligned}$$

The relations between the constants A_1, B_1 etc. are now given by

$$(17) \quad \begin{aligned} q_1 B_1 &= A_1, & q_1 B_2 &= -A_2, \\ q_2 B_3 &= A_3, & q_2 B_4 &= -A_4 \end{aligned}$$

and the displacements by

$$(18) \quad u = -2k \sin kx e^{ipt} [A_1 e^{q_1 z} + A_2 e^{-q_1 z} + A_3 e^{q_2 z} + A_4 e^{-q_2 z}],$$

$$(19) \quad \omega = 2 \cos kx e^{ipt} [q_1 A_1 e^{q_1 z} - q_1 A_2 e^{-q_1 z} + q_2 A_3 e^{q_2 z} - q_2 A_4 e^{-q_2 z}].$$

Case (i). For a semi-infinite medium of cubic material, the suitable solutions for u and ω as obtained from (13) and (14) in case (A) are

$$(20) \quad u = -k \sin kx e^{ipt} [(1 + \xi) A_2 e^{-q_1 z} + (1 + \eta) A_4 e^{-q_2 z}],$$

$$(21) \quad \omega = -\cos kx e^{ipt} \left[\left\{ q_1 + \left(\frac{q_1^2 + \alpha}{q_1} \right) \xi \right\} A_2 e^{-q_1 z} + \left\{ q_2 + \left(\frac{q_2^2 + \alpha}{q_2} \right) \eta \right\} A_4 e^{-q_2 z} \right].$$

The stress-strain relations give

$$(22) \quad \widehat{z z} = c_{12} \frac{\partial u}{\partial x} + c_{11} \frac{\partial \omega}{\partial z},$$

$$\widehat{z x} = c_{44} \left(\frac{\partial u}{\partial z} + \frac{\partial \omega}{\partial x} \right).$$

The boundary conditions require that the stress-components $\widehat{z z}$ and $\widehat{z x}$ vanish at $z = 0$. These conditions together with (20), (21) and (22) yield

$$(23) \quad A_2 [c_{11} \{q_1^2 + (q_1^2 + \alpha) \xi\} - c_{12} k^2 (1 + \xi)] + A_4 [c_{11} \{q_2^2 + (q_2^2 + \alpha) \eta\} - c_{12} k^2 (1 + \eta)] = 0,$$

$$(24) \quad A_2 [q_1 (1 + \xi) + 1/q_1 \{q_1^2 + (q_1^2 + \alpha) \xi\}] + A_4 [q_2 (1 + \eta) + 1/q_2 \{q_2^2 + (q_2^2 + \alpha) \eta\}] = 0.$$

Eliminating A_2 and A_4 from (23) and (24) we get the frequency equations as

$$(25) \quad [c_{11} \{q_1^2 + (q_1^2 + \alpha) \xi - c_{12} k^2 (1 + \xi)\} [q_2 (1 + \eta) + 1/q_2 \{q_2^2 + (q_2^2 + \alpha) \eta\}] - [c_{11} \{q_2^2 + (q_2^2 + \alpha) \eta\} - c_{12} k^2 (1 + \eta)] [q_1 (1 + \xi) + 1/q_1 \{q_1^2 + (q_1^2 + \alpha) \xi\}] = 0.$$

Again, if we take the values of q_1 and q_2 as obtained from (16) in case (B) the frequency equation becomes

$$(26) \quad \left(\frac{\rho c^2}{c_{44}} \right)^2 - \left(\frac{c_{11} + c_{12}}{c_{44}} + 2 \right) \left(\frac{\rho c^2}{c_{44}} \right) + \left(2 + \frac{c_{12}}{c_{44}} \right) \left(\frac{c_{11}}{c_{44}} - \frac{c_{12}^2}{c_{11} c_{44}} \right) = 0.$$

Case (ii). For a layer of the cubic material of finite thickness h resting on a rigid base, the boundary conditions are

$$(27) \quad \widehat{z z} = 0, \quad \widehat{z x} = 0 \quad \text{at } z = 0,$$

$$u = 0, \quad \omega = 0 \quad \text{at } z = h.$$

These boundary conditions together with (18), (19) and (22) give

$$(28) \quad \begin{aligned} l_1 A_1 + l_1 A_2 + l_2 A_3 + l_2 A_4 &= 0, \\ q_1 A_1 - q_1 A_2 + q_2 A_3 - q_2 A_4 &= 0, \\ A_1 e^{q_1 h} + A_2 e^{-q_1 h} + A_3 e^{q_2 h} + A_4 e^{-q_2 h} &= 0, \\ A_1 q_1 e^{q_1 h} - A_2 q_1 e^{-q_1 h} + A_3 q_2 e^{q_2 h} - A_4 q_2 e^{-q_2 h} &= 0, \end{aligned}$$

where

$$(29) \quad \begin{aligned} l_1 &= k^2 c_{12} - q_1^2 c_{11}, \\ l_2 &= k^2 c_{12} - q_2^2 c_{11} \end{aligned}$$

and q_1 and q_2 are given by (16).

Eliminating A_1, A_2, A_3, A_4 from equations (28), we get the frequency equation

$$(30) \quad \begin{vmatrix} l_1 & l_1 & l_2 & l_2 \\ q_1 & -q_1 & q_2 & -q_2 \\ e^{q_1 h} & e^{-q_1 h} & e^{q_2 h} & e^{-q_2 h} \\ q_1 e^{q_1 h} & -q_1 e^{-q_1 h} & q_2 e^{q_2 h} & -q_2 e^{-q_2 h} \end{vmatrix} = 0.$$

Case (iii). Let us now consider an isotropic homogeneous semi-infinite medium overlaid by a layer of the cubic material of finite thickness h .

The equations of motion for the lower isotropic medium in two dimensions are

$$(31) \quad (\lambda_1 + u_1) \frac{\partial \Delta}{\partial x} + \mu_1 \left(\frac{\partial^2 u_1}{\partial x^2} + \frac{\partial^2 u_1}{\partial z^2} \right) = \rho_1 \frac{\partial^2 u_1}{\partial t^2},$$

$$(32) \quad (\lambda_1 + \mu_1) \frac{\partial \Delta}{\partial z} + \mu_1 \left(\frac{\partial^2 \omega_1}{\partial x^2} + \frac{\partial^2 \omega_1}{\partial z^2} \right) = \rho_1 \frac{\partial^2 \omega_1}{\partial t^2},$$

where u_1 and ω_1 are the displacement components in the lower medium, ρ_1 and μ_1 are respectively the density and the rigidity, and

$$\Delta = \frac{\partial u_1}{\partial x} + \frac{\partial \omega_1}{\partial z}.$$

Substituting

$$(33) \quad \begin{aligned} u_1 &= \frac{\partial \varphi_1}{\partial x} + \frac{\partial \psi_1}{\partial z}, \\ \omega_1 &= \frac{\partial \varphi_1}{\partial z} - \frac{\partial \psi_1}{\partial x}, \end{aligned}$$

in (31) and (32), we find that these equations are satisfied if

$$(34) \quad \frac{\partial^2 \varphi_1}{\partial x^2} + \frac{\partial^2 \varphi_1}{\partial z^2} = \frac{1}{\alpha_1^2} \frac{\partial^2 \varphi_1}{\partial t^2}$$

and

$$(35) \quad \frac{\partial^2 \psi_1}{\partial x^2} + \frac{\partial^2 \psi_1}{\partial z^2} = \frac{1}{\beta_1^2} \frac{\partial^2 \psi_1}{\partial t^2},$$

where

$$(36) \quad \alpha_1 = \left(\frac{\lambda_1 + 2\mu_1}{\rho_1} \right)^{1/2}, \quad \beta_1 = \left(\frac{\mu_1}{\rho_1} \right)^{1/2}.$$

The solutions of equations (34) and (35) suitable for the problem are

$$(37) \quad \begin{aligned} \varphi_1 &= L_1 e^{-n_1 z} \cos kx e^{ipt}, \\ \psi_1 &= M_1 e^{-n_2 z} \sin kx e^{ipt}, \end{aligned}$$

where

$$(38) \quad \begin{aligned} n_1 &= k \sqrt{(1 - c^2/\alpha_1^2)}, \\ n_2 &= k \sqrt{(1 - c^2/\beta_1^2)}. \end{aligned}$$

The stress-components are given by

$$(39) \quad \begin{aligned} (\widehat{zz})_1 &= \lambda_1 \frac{\partial u_1}{\partial x} + (\lambda_1 + 2\mu_1) \frac{\partial \omega_1}{\partial z}, \\ (\widehat{zx})_1 &= \mu_1 \left(\frac{\partial u_1}{\partial z} + \frac{\partial \omega_1}{\partial x} \right). \end{aligned}$$

The boundary conditions in this case are

$$(40) \quad \begin{aligned} \widehat{zz} &= 0, \quad \widehat{zx} = 0 \quad \text{at } z = 0 \\ u &= u_1, \quad \omega = \omega_1 \\ \widehat{zz} &= (\widehat{zz})_1, \quad \widehat{zx} = (\widehat{zx})_1 \quad \text{at } z = h. \end{aligned}$$

These conditions lead to

$$\begin{aligned} l_1 A_1 + l_1 A_2 + l_2 A_3 + l_2 A_4 &= 0, \\ q_1 A_1 - q_1 A_2 + q_2 A_3 - q_2 A_4 &= 0, \\ 2e^{q_1 h} A_1 + 2e^{-q_1 h} A_2 + 2e^{q_2 h} A_3 + 2e^{-q_2 h} A_4 - L_1 e^{-n_1 h} - \frac{M_1}{k} n_2 e^{-n_2 h} &= 0, \\ 2q_1 e^{q_1 h} A_1 - 2q_1 e^{-q_1 h} A_2 + 2q_2 e^{q_2 h} A_3 - 2q_2 e^{-q_2 h} A_4 + L_1 n_1 e^{-n_1 h} + \\ &\quad + M_1 k e^{-n_2 h} = 0, \\ -2l_1 e^{q_1 h} A_1 - 2l_1 e^{-q_1 h} A_2 - 2l_2 e^{q_2 h} A_3 - 2l_2 e^{-q_2 h} A_4 - m_1 e^{-n_1 h} L_1 - \\ &\quad - 2\mu_1 \alpha_1 n_2 e^{-n_2 h} M_1 = 0, \\ -2kc_{44} q_1 e^{q_1 h} A_1 + 2kc_{44} q_1 e^{-q_1 h} A_2 - 2kc_{44} q_2 e^{q_2 h} A_3 + \\ &\quad + 2kc_{44} q_2 e^{-q_2 h} A_4 - 2\mu_1 k n_1 e^{-n_1 h} L_1 - \mu_1 (n_2^2 + k^2) e^{-n_2 h} M_1 = 0, \end{aligned}$$

where

$$(41) \quad m_1 = \lambda(n_1^2 - k^2) + 2\mu_1 n_1^2$$

and q_1, q_2 are given by (16).

Eliminating A_1, A_2, A_3, A_4, L_1 and M_1 from these relations we get

$$(42) \quad \begin{vmatrix} l_1 & l_1 & l_2 & l_2 \\ q_1 & -q_1 & q_2 & -q_2 \\ 2e^{q_1 h} & 2e^{-q_1 h} & 2e^{q_2 h} & 2e^{-q_2 h} \\ 2q_1 e^{q_1 h} & -2q_1 e^{-q_1 h} & 2q_2 e^{q_2 h} & -2q_2 e^{-q_2 h} \\ -2l_1 e^{q_1 h} & -2l_1 e^{-q_1 h} & -2l_2 e^{q_2 h} & -2l_2 e^{-q_2 h} \\ -2kc_{44}q_1 e^{q_1 h} & 2kc_{44}q_1 e^{-q_1 h} & -2kc_{44}q_2 e^{q_2 h} & 2kc_{44}q_2 e^{-q_2 h} \\ 0 & 0 \\ 0 & 0 \\ -e^{-n_1 h} & -n_2/k e^{-n_2 h} \\ n_1 e^{-n_1 h} & k e^{-n_2 h} \\ -m_1 e^{-n_1 h} & -2\mu_1 \alpha_1 n_2 e^{-n_2 h} \\ -2\mu_1 k_1 n_1 e^{-n_1 h} & -\mu_1 (n_2^2 + k^2) e^{-n_2 h} \end{vmatrix} = 0$$

NUMERICAL RESULTS

For numerical calculation of the roots of the frequency equations, we take the values of the elastic constants to be those for pyrites, i.e.

$$\begin{aligned} c_{11} &= 3680 \times 10^6 \text{ grammes wt. per sq. cm.} \\ c_{44} &= 1075 \times 10^6 \text{ grammes wt. per sq. cm.} \\ c_{12} &= -483 \times 10^6 \text{ grammes wt. per sq. cm.} \end{aligned}$$

Roots of equation (25). (Approximate Solution.) Let us choose α to be so small that $q_1^2 + \alpha \simeq q_1^2$, $q_2^2 + \alpha \simeq q_2^2$,

$$(c_{12} + 2c_{44})q_1^2 + \varrho p^2 - c_{11}k^2 + (c_{12} + c_{44})\alpha \simeq (c_{12} + 2c_{44})q_1^2 + \varrho p^2 - c_{11}k^2$$

and

$$(c_{12} + 2c_{44})q_2^2 + \varrho p^2 - c_{11}k^2 + (c_{12} + c_{44})\alpha \simeq (c_{12} + 2c_{44})q_2^2 + \varrho p^2 - c_{11}k^2,$$

so that $\xi = 1$ and $\eta = 1$.

Equation (25) with the values of q_1 and q_2 given by equation (9) in (A) then reduces to

$$\left(\frac{c^2}{\beta^2}\right)^2 - \left(\frac{c_{11}}{c_{44}} + 1\right)\left(\frac{c^2}{\beta^2}\right) + \left(\frac{c_{11}}{c_{44}} - \frac{c_{12}^2}{c_{11}c_{44}}\right) = 0$$

where

$$\frac{c^2}{\beta^2} = \frac{\rho c^2}{c_{44}}.$$

Hence

$$\frac{c}{\beta} = \left[\frac{1}{2} \left(\frac{c_{11}}{c_{44}} + 1 \pm \left\{ \left(\frac{c_{11}}{c_{44}} - 1 \right)^2 + 4 \frac{c_{12}^2}{c_{11}c_{44}} \right\}^{1/2} \right) \right]^{1/2}.$$

With the values of the elastic constants given above, we get

$$c/\beta = 0.987, 1.85.$$

The former of these two values of c/β clearly corresponds to Rayleigh waves.

We, therefore, conclude that Rayleigh waves exist in a semi-infinite medium of aeolotropic material with cubic symmetry.

Roots of equation (26)

Here

$$\begin{aligned} \frac{c}{\beta} = & \left[\frac{1}{2} \left(\frac{c_{11} + c_{12}}{c_{44}} + 2 \pm \left\{ \left(\frac{c_{11} + c_{12}}{c_{44}} + 2 \right)^2 - \right. \right. \right. \\ & \left. \left. \left. - 4 \left(2 + \frac{c_{12}}{c_{44}} \right) \left(\frac{c_{11}}{c_{44}} - \frac{c_{12}^2}{c_{11}c_{44}} \right) \right\}^{1/2} \right) \right]^{1/2}. \end{aligned}$$

Hence $c/\beta = 1.23, 1.86$.

Roots of equation (30)

Four of the roots of the equation are readily obtained as

$$\frac{c}{\beta} = \left(2 + \frac{c_{12}}{c_{44}} \right)^{1/2}, \quad 2^{1/2}, \quad \left(\frac{c_{11}^2 - c_{12}^2 - 2c_{12}c_{44}}{c_{11}c_{44}} \right)^{1/2}, \quad \left(\frac{c_{11}}{c_{44}} \right)^{1/2}.$$

Hence four of the roots are

$$c/\beta = 1.24, 1.41, 1.90 \text{ and } 2.03.$$

Roots of equation (42)

Two of the roots are easily found to be

$$\frac{c}{\beta} = \left(2 + \frac{c_{12}}{c_{44}} \right)^{1/2}, \quad \left(\frac{c_{11}}{c_{44}} \right)^{1/2}.$$

Hence $c/\beta = 1.24, 2.03$.

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Souhrn

ŠÍŘENÍ VLN RAYLEIGHOVA TYPU V AELOTROPICKÉM
MATERIÁLU S KUBICKOU SYMETRIÍ

SUBHAS DUTTA a PRIYATOSH ROY

V článku se zkoumá možnost šíření vln Rayleighova typu v aeotropickém materiálu kubického systému pro různé modely.

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