

# Aplikace matematiky

---

Alexander Hanuška

The Reissnerian algorithms in the refined theories of the bending of plates

*Aplikace matematiky*, Vol. 13 (1968), No. 6, 441–455

Persistent URL: <http://dml.cz/dmlcz/103194>

## Terms of use:

© Institute of Mathematics AS CR, 1968

Institute of Mathematics of the Czech Academy of Sciences provides access to digitized documents strictly for personal use. Each copy of any part of this document must contain these *Terms of use*.



This document has been digitized, optimized for electronic delivery and stamped with digital signature within the project *DML-CZ: The Czech Digital Mathematics Library* <http://dml.cz>

THE REISSNERIAN ALGORITHMS IN THE REFINED THEORIES  
OF THE BENDING OF PLATES

ALEXANDER HANUŠKA

(Received February 1, 1967)

In this paper equations are derived for the bending of plates, that represent a certain generalization of the refined theories presented by I. BABUŠKA and M. PRÁGER [1–4]. The authors have shown that by accepting the notion of an asymptotical energetic error it is possible to find a unique algorithm (called by the authors “the Reissnerian algorithm”) of the gradual refinement of Kirchhoff’s technical plate theory. In the following is derived a differential equation of infinite order which is formally related to Lurje’s equations [5, 6], and the boundary conditions, which in the given case correspond to the solution of the so called internal problem (the fundamental state of stress), are clarified [7, 8].

An outline of the important results obtained by the various authors is given by the survey papers [9–12].

**1.** In the works [1–4] it has been shown that if the displacements  $u, v, w$  are approximated in the form of finite series

$$(1.1) \quad \begin{aligned} u_N(x, y, h\zeta) &= \sum_{i=1}^N (-1)^{i-1} h^{2i-1} a_i(x, y) \varphi_i^0(\zeta), \\ v_N(x, y, h\zeta) &= \sum_{i=1}^N (-1)^{i-1} h^{2i-1} b_i(x, y) \varphi_i^0(\zeta), \\ w_N(x, y, h\zeta) &= \sum_{i=1}^{N+1} (-1)^{i-1} h^{2i-2} c_i(x, y) \psi_i^0(\zeta), \end{aligned}$$

where  $2h$  denotes the thickness of the plate,  $a_i, b_i$  and  $c_i$  are the solutions of the respective Eulerian equations, and  $\varphi_i^0$  and  $\psi_i^0$  are certain “optimum” polynomials, the energetic error of this approximate solution, when compared with the exact solution of the threedimensional equations of Lamé, will – for a whole class of functions expressing the loading – be minimum. The optimum functions  $\varphi_i^0$  and  $\psi_i^0$  represent polynomials and have been derived in [1]. Some of their first values,

required further, are

$$\begin{aligned}
 (1.2) \quad & \varphi_1^0 = -\gamma\zeta, & \psi_1^0 = \gamma, \\
 & \varphi_2^0 = \frac{10 - 3\gamma}{10}\zeta - \frac{\gamma + 2}{6}\zeta^3, & \psi_2^0 = \frac{10 + 3\gamma}{10} + \frac{\gamma - 2}{2}\zeta^2, \\
 & \varphi_3^0 = \frac{157\gamma - 140}{4200}\zeta + \frac{4 - 3\gamma}{60}\zeta^3 - & \psi_3^0 = -\frac{157\gamma + 140}{4200} + \frac{4 + 3\gamma}{20}\zeta^2 + \\
 & - \frac{\gamma + 4}{120}\zeta^5, & + \frac{\gamma - 4}{24}\zeta^4, \\
 & & \psi_4^0 = \frac{569\gamma - 1020}{252\,000} + \\
 & & + \frac{174 - 157\gamma}{8400}\zeta^2 + \\
 & & + \frac{3\gamma - 2}{240}\zeta^4 + \frac{\gamma - 6}{720}\zeta^6,
 \end{aligned}$$

where

$$(1.3) \quad \gamma = 2(1 - v)$$

and  $v$  is Poisson's ratio.

In this paper we shall be concerned with a special case when the functions  $a_i$ ,  $b_i$  and  $c_i$  may be expressed in the following manner

$$(1.4) \quad a_i(x, y) = \frac{\partial \Delta^{i-1} w_0(x, y)}{\partial x}, \quad b_i(x, y) = \frac{\partial \Delta^{i-1} w_0(x, y)}{\partial y}, \quad c_i(x, y) = \Delta^{i-1} w_0(x, y),$$

where  $\Delta$  denotes the twodimensional Laplace operator.

When substituting equation (1.2) and (1.3) into equation (1.1) we can see that the obtained formulas for the displacements are formally identical with the expansions, the first two members of which were determined by L. H. DONNEL in a different way [14].

It may be shown that if in the series for displacements obtained in such a manner, we consider the limit  $N \rightarrow \infty$ , it is then possible to sum up these series formally and we shall obtain

$$\begin{aligned}
 (1.5) \quad u(x, y, h\zeta) &= \sum_{i=1}^{\infty} (-1)^{i-1} h^{2i-1} \varphi_i^0 \frac{\partial \Delta^{i-1} w_0}{\partial x} = \frac{4}{3} h^3 \frac{\partial L_1 w_0}{\partial x}, \\
 v(x, y, h\zeta) &= \sum_{i=1}^{\infty} (-1)^{i-1} h^{2i-1} \varphi_i^0 \frac{\partial \Delta^{i-1} w_0}{\partial y} = \frac{4}{3} h^3 \frac{\partial L_1 w_0}{\partial y}, \\
 w(x, y, h\zeta) &= \sum_{i=1}^{\infty} (-1)^{i-1} h^{2i-2} \psi_i^0 \Delta^{i-1} w_0 = \frac{4}{3} h^3 L_2 w_0,
 \end{aligned}$$

where  $L_1$  and  $L_2$  are partial differential operators of infinite order, which are regular in the sense of [15]

(1.6)

$$L_1(\sqrt{A}h, \zeta) = [\sqrt{A}h \sin \sqrt{A}h \sin \sqrt{A}h\zeta + \sqrt{A}h\zeta \cos \sqrt{A}h \cos \sqrt{A}h\zeta + \\ + (\gamma - 1) \cos \sqrt{A}h \sin \sqrt{A}h\zeta] \frac{\sqrt{A}}{\sin 2\sqrt{A}h - 2\sqrt{A}h},$$

$$L_2(\sqrt{A}h, \zeta) = [\sqrt{A}h \sin \sqrt{A}h \cos \sqrt{A}h\zeta - \sqrt{A}h\zeta \cos \sqrt{A}h \sin \sqrt{A}h\zeta - \\ - \gamma \cos \sqrt{A}h \cos \sqrt{A}h\zeta] \frac{\sqrt{A}\sqrt{A}}{\sin 2\sqrt{A}h - 2\sqrt{A}h}.$$

Starting from equations (1.5) we derive the differential equation of the problem and we make clear the form of the corresponding boundary conditions. For this purpose it will be useful to apply the Lagrange variational principle.

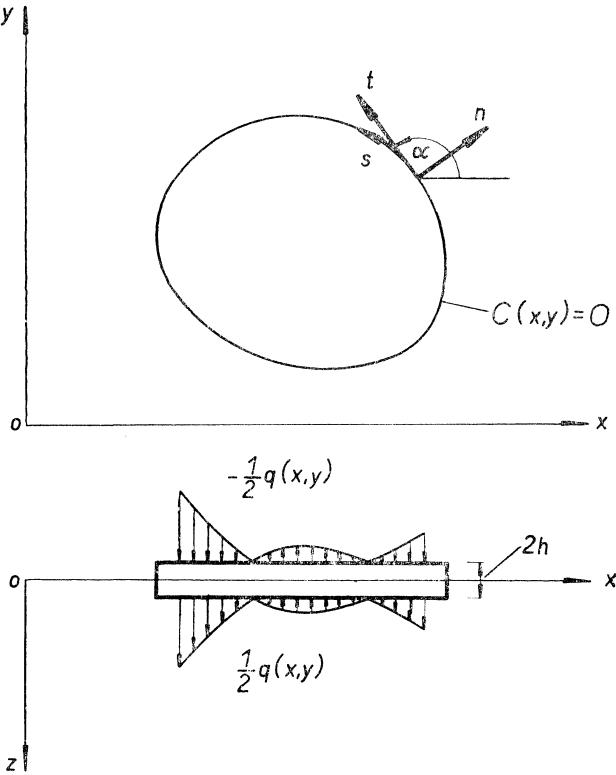


Fig. 1.

Let us assume that on the upper and the lower plane of the plate (Fig. 1), only a normal load  $\pm \frac{1}{2}q(x, y)$  is acting and on the cylindrical surface of the boundary  $C(x, y) = 0$  the homogeneous boundary conditions are prescribed. The potential energy of the plate will then be given by formula [16]

$$(1.7) \quad V = \frac{1}{2} \iiint_{-1}^1 \left\{ \lambda \left( \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{h \partial \zeta} \right)^2 + 2\mu \left[ \left( \frac{\partial u}{\partial x} \right)^2 + \left( \frac{\partial v}{\partial y} \right)^2 + \left( \frac{\partial w}{h \partial \zeta} \right)^2 \right] + \right. \\ \left. + \mu \left[ \left( \frac{\partial w}{\partial y} + \frac{\partial v}{h \partial \zeta} \right)^2 + \left( \frac{\partial u}{h \partial \zeta} + \frac{\partial w}{\partial x} \right)^2 + \left( \frac{\partial v}{\partial x} + \frac{\partial u}{\partial y} \right)^2 \right] \right\} dx dy h d\zeta - \\ - \iint w(x, y, h) \cdot \frac{1}{2}q(x, y) + w(x, y, -h) \cdot \frac{1}{2}q(x, y) ] dx dy < \infty .$$

In this equation  $\lambda$  and  $\mu$  are Lamé's constants.

From the Lagrange principle it follows that  $\delta V = 0$ , from which it is

$$(1.8) \quad \iiint_{-1}^1 \left\{ \frac{\lambda}{\mu} \left( \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{h \partial \zeta} \right) \left( \frac{\partial \delta u}{\partial x} + \frac{\partial \delta v}{\partial y} + \frac{\partial \delta w}{h \partial \zeta} \right) + \right. \\ + 2 \left( \frac{\partial u}{\partial x} \frac{\partial \delta u}{\partial x} + \frac{\partial v}{\partial y} \frac{\partial \delta v}{\partial y} + \frac{\partial w}{h \partial \zeta} \frac{\partial \delta w}{h \partial \zeta} \right) + \left( \frac{\partial w}{\partial y} + \frac{\partial v}{h \partial \zeta} \right) \left( \frac{\partial \delta w}{\partial y} + \frac{\partial \delta v}{h \partial \zeta} \right) + \\ + \left( \frac{\partial u}{h \partial \zeta} + \frac{\partial w}{\partial x} \right) \left( \frac{\partial \delta u}{h \partial \zeta} + \frac{\partial \delta w}{\partial x} \right) + \left( \frac{\partial v}{\partial x} + \frac{\partial u}{\partial y} \right) \left( \frac{\partial \delta v}{\partial x} + \frac{\partial \delta u}{\partial y} \right) \Big] h d\zeta - \\ \left. - \frac{1}{\mu} q \delta w(x, y, h) \right\} dx dy = 0 .$$

When (1.5) is substituted into (1.8) and the relation

$$(1.9) \quad \frac{\lambda}{\mu} = \frac{2 - \gamma}{\gamma - 1}$$

is used, we obtain

$$(1.10) \quad \iiint_{-1}^1 \left\{ \frac{2 - \gamma}{\gamma - 1} \left( L_1 A + \frac{\partial L_2}{h \partial \zeta} \right) w_0 \cdot \left( L_1 A + \frac{\partial L_2}{h \partial \zeta} \right) \delta w_0 + 2 \frac{\partial L_2 w_0}{h \partial \zeta} \cdot \frac{\partial L_2 \delta w_0}{h \partial \zeta} + \right. \\ + \frac{\partial}{\partial x} \left( \frac{\partial L_1}{h \partial \zeta} + L_2 \right) w_0 \cdot \frac{\partial}{\partial x} \left( \frac{\partial L_1}{h \partial \zeta} + L_2 \right) \delta w_0 + \frac{\partial}{\partial y} \left( \frac{\partial L_1}{h \partial \zeta} + L_2 \right) w_0 \cdot \\ \cdot \frac{\partial}{\partial y} \left( \frac{\partial L_1}{h \partial \zeta} + L_2 \right) \delta w_0 + 2 \left( \frac{\partial^2 L_1 w_0}{\partial x^2} \cdot \frac{\partial^2 L_1 \delta w_0}{\partial x^2} + 2 \frac{\partial^2 L_1 w_0}{\partial x \partial y} \cdot \frac{\partial^2 L_1 \delta w_0}{\partial x \partial y} + \right. \\ \left. + \frac{\partial^2 L_1 w_0}{\partial y^2} \cdot \frac{\partial^2 L_1 \delta w_0}{\partial y^2} \right) \Big] h d\zeta - \frac{q(x, y)}{D(1 - \nu)} L_2(\sqrt(A)h, 1) \delta w_0 \right\} dx dy = 0 ,$$

where  $D$  is the flexural rigidity of the plate according to the technical theory of plates

$$(1.11) \quad D = \frac{4}{3} \frac{\mu h^3}{1 - \nu} = \frac{8\mu h^3}{3\nu}.$$

It is important to point out the meaning of the points in (1.10) because they indicate the limit of the action of the corresponding operator. In the equation (1.10) there are terms containing the values of operators of the variations of  $w_0$ . We, however, need the variations of the function  $w_0$  itself and of its normal derivatives. Such an arrangement of the equation (1.10) is possible by using the formula derived by V. K. PROKOPOV [17]. According to this it holds

$$(1.12) \quad \iint U \cdot X(\Delta) V \cdot dx dy = \iint X(\Delta) U \cdot V \cdot dx dy + \sum_{k=1}^{\infty} \int_C \left\{ X^{(k)}(\Delta) U \cdot \frac{\partial \Delta^{k-1} V}{\partial n} - \frac{\partial X^{(k)}(\Delta) U}{\partial n} \cdot \Delta^{k-1} V \right\} ds.$$

In this equation  $X(\Delta)$  is the differential operator

$$(1.13) \quad X(\Delta) = \sum_{j=0}^{\infty} a_j \Delta^j,$$

and  $X^{(k)}(\Delta)$  is the so called  $k$ -th reduced operator

$$(1.14) \quad X^{(k)}(\Delta) = \sum_{j=k}^{\infty} a_j \Delta^{j-k}.$$

The relation (1.12) is a generalisation of Green's formula

$$(1.15) \quad \iint U \cdot \Delta V \cdot dx dy = \iint \Delta U \cdot V \cdot dx dy + \int_C \left( U \cdot \frac{\partial V}{\partial n} - \frac{\partial U}{\partial n} \cdot V \right) ds.$$

Using, in equation (1.10), Green's generalized formula (1.12), the ordinary Green formula (1.15) and an integration by parts, we obtain

$$(1.16) \quad \begin{aligned} & \frac{2-\gamma}{\gamma-1} \iiint_{-1}^1 \left( \Delta L_1 + \frac{\partial L_2}{h \partial \zeta} \right)^2 w_0 \cdot \delta w_0 \, dx \, dy \, h \, d\zeta + \frac{2-\gamma}{\gamma-1} \int_C \int_{-1}^1 \left\{ \left( \Delta L_1 + \frac{\partial L_2}{h \partial \zeta} \right) w_0 \cdot \right. \\ & \cdot \frac{\partial L_1 \delta w_0}{\partial n} - \frac{\partial}{\partial n} \left( \Delta L_1 + \frac{\partial L_2}{h \partial \zeta} \right) w_0 \cdot L_1 \delta w_0 + \sum_{k=1}^{\infty} \left[ \left( \Delta L_1^{(k)} + \frac{\partial L_2^{(k)}}{h \partial \zeta} \right) \left( \Delta L_1 + \frac{\partial L_2}{h \partial \zeta} \right) w_0 \cdot \right. \\ & \cdot \left. \frac{\partial \Delta^{k-1} \delta w_0}{\partial n} - \frac{\partial}{\partial n} \left( \Delta L_1^{(k)} + \frac{\partial L_2^{(k)}}{h \partial \zeta} \right) \left( \Delta L_1 + \frac{\partial L_2}{h \partial \zeta} \right) w_0 \cdot \Delta^{k-1} \delta w_0 \right] \left. \right\} ds \, h \, d\zeta + \\ & + 2 \iiint_{-1}^1 \left( \frac{\partial L_2}{h \partial \zeta} \right)^2 w_0 \cdot \delta w_0 \, dx \, dy \, h \, d\zeta + 2 \int_C \int_{-1}^1 \sum_{k=1}^{\infty} \left( \frac{\partial L_2^{(k)}}{h \partial \zeta} \frac{\partial L_2}{h \partial \zeta} w_0 \cdot \frac{\partial \Delta^{k-1} \delta w_0}{\partial n} - \right. \end{aligned}$$

$$\begin{aligned}
& - \frac{\partial}{\partial n} \frac{\partial L_2^{(k)}}{\partial \zeta} \frac{\partial L_2}{\partial \zeta} w_0 \cdot A^{k-1} \delta w_0 \Big) ds h d\zeta - \iiint_{-1}^1 A \left( \frac{\partial L_1}{\partial \zeta} + L_2 \right)^2 w_0 \cdot \delta w_0 dx dy h d\zeta + \\
& + \int_C \int_{-1}^1 \left\{ \frac{\partial}{\partial n} \left( \frac{\partial L_1}{\partial \zeta} + L_2 \right) w_0 \cdot \left( \frac{\partial L_1}{\partial \zeta} + L_2 \right) \delta w_0 - \sum_{k=1}^{\infty} \left[ A \left( \frac{\partial L_1^{(k)}}{\partial \zeta} + L_2^{(k)} \right) \right. \right. \\
& \cdot \left( \frac{\partial L_1}{\partial \zeta} + L_2 \right) w_0 \cdot \frac{\partial A^{k-1} \delta w_0}{\partial n} - \frac{\partial}{\partial n} A \cdot \left( \frac{\partial L_1^{(k)}}{\partial \zeta} + L_2^{(k)} \right) \left( \frac{\partial L_1}{\partial \zeta} + L_2 \right) w_0 \cdot A^{k-1} \delta w_0 \Big] \Big\} \cdot \\
& \cdot ds h d\zeta + 2 \iiint_{-1}^1 A^2 L_1^{(k)} w_0 \cdot \delta w_0 dx dy h d\zeta + 2 \int_C \int_{-1}^1 \left[ \frac{\partial^2 L_1 w_0}{\partial n^2} \cdot \frac{\partial L_1 \delta w_0}{\partial n} + \right. \\
& + \left( \frac{\partial^2 L_1}{\partial n \partial s} - \frac{\partial \alpha}{\partial s} \frac{\partial L_1}{\partial s} \right) w_0 \cdot \frac{\partial L_1 \delta w_0}{\partial s} - \frac{\partial}{\partial n} A L_1 w_0 \cdot L_1 \delta w_0 + \sum_{k=1}^{\infty} \left( A^2 L_1^{(k)} L_1 w_0 \cdot \right. \\
& \left. \left. \frac{\partial A^{k-1} \delta w_0}{\partial n} - \frac{\partial}{\partial n} A^2 L_1^{(k)} L_1 w_0 \cdot A^{k-1} \delta w_0 \right) \right] ds dh d\zeta - \frac{2}{\gamma D} \left\{ \iiint_{-1}^1 L_2(\sqrt(A) h, 1) q \cdot \right. \\
& \cdot \delta w_0 dx dy h d\zeta + \int_C \int_{-1}^1 \sum_{k=1}^{\infty} \left[ L_2^{(k)}(\sqrt(A) h, 1) q \cdot \frac{\partial A^{k-1} \delta w_0}{\partial n} - \right. \\
& \left. \left. - \frac{\partial}{\partial n} L_2^{(k)}((\sqrt(A) h, 1) q \cdot A^{k-1} \delta w_0) \right] ds h d\zeta \right\} = 0.
\end{aligned}$$

In this equation the operators  $L_1$  and  $L_2$  are given in their finite form by equation (1.6). For further calculations, their form in series following from equation (1.5) is also advantageous:

$$\begin{aligned}
(1.17) \quad L_1(\sqrt(A) h, \zeta) &= \frac{3}{4h^2} \sum_{j=0}^{\infty} (-1)^j (\sqrt(A) h)^{2j} \varphi_{j+1}^0(\zeta), \\
L_2(\sqrt(A) h, \zeta) &= \frac{3}{4h^3} \sum_{j=0}^{\infty} (-1)^j (\sqrt(A) h)^{2j} \psi_{j+1}^0(\zeta).
\end{aligned}$$

The reduced operators  $L_1^{(k)}$  and  $L_2^{(k)}$ , according to the definition (1.14) will be

$$\begin{aligned}
(1.18) \quad L_1^{(k)}(\sqrt(A) h, \zeta) &= \frac{3}{4} h^{2k-2} \sum_{j=0}^{\infty} (-1)^{j+k} (\sqrt(A) h)^{2j} \varphi_{j+k+1}^0(\zeta), \\
L_2^{(k)}(\sqrt(A) h, \zeta) &= \frac{3}{4} h^{2k-3} \sum_{j=0}^{\infty} (-1)^{j+k} (\sqrt(A) h)^{2j} \psi_{j+k+1}^0(\zeta).
\end{aligned}$$

Further in equation (1.16)  $\alpha$  is the angle between the tangent to the curve  $C(x, y) = 0$ , and the axis  $x$  (Fig. 1), and  $\partial \alpha / \partial s$  is the curvature of the boundary  $C$ . The Laplace operator in the line integrals is

$$(1.19) \quad A = \frac{\partial^2}{\partial n^2} + \frac{\partial^2}{\partial t^2} = \frac{\partial^2}{\partial n^2} + \frac{\partial \alpha}{\partial s} \frac{\partial}{\partial n} + \frac{\partial^2}{\partial s^2}.$$

With regard to the arbitrariness of  $\delta w_0$  the members with the volume integrals in (1.16) will be equal to zero

(1.20)

$$\iiint \left\{ \int_{-1}^1 \left[ \frac{2-\gamma}{\gamma-1} \left( L_1 A + \frac{\partial L_2}{h \partial \zeta} \right)^2 + 2 \left( \frac{\partial L_2}{h \partial \zeta} \right)^2 - \left( \frac{\partial L_1}{h \partial \zeta} + L_2 \right)^2 A + 2L_1^2 A \right] w_0 \cdot h d\zeta - \right. \\ \left. - \frac{2}{\gamma D} L_2(\sqrt(A) h, 1) q \right\} \delta w_0 dx dy = 0.$$

When substituting for  $L_1$  and  $L_2$  the expressions (1.5), and taking  $A$  as a number, the expressions in (1.20) can be integrated with respect to  $\zeta$ . We are not giving here cumbersome calculations, we only present the final result

(1.21)

$$\iint \left[ -2\gamma \frac{A \sqrt(A) \cos^2 \sqrt(A) h}{\sin 2 \sqrt(A) h - 2 \sqrt(A) h} A^2 w_0 + \frac{\gamma}{(1-v) D} \frac{A \sqrt(A) \cos^2 \sqrt(A) h}{\sin 2 \sqrt(A) h - 2 \sqrt(A) h} q \right] \\ \cdot \delta w_0 dx dy = 0.$$

With regard to the arbitrariness of  $\delta w_0$  the expression under the integral must be equal to zero. From the latter we obtain the basic differential equation of a variant of the refined Babuška-Práger theory

$$(1.22) \quad \frac{A \sqrt(A) \cos^2 \sqrt(A) h}{\sin 2 \sqrt(A) h - 2 \sqrt(A) h} \left[ A^2 w_0 - \frac{q}{2(1-v) D} \right] = 0.$$

The transcendental differential operator standing before the bracket is then  $-(1/\gamma) L_2(\sqrt(A) h, 1)$  and thus using (1.17) we can write the equation (1.22) in the form of a differential equation of infinite order

$$(1.23) \quad \sum_{j=1}^{\infty} \frac{1}{\gamma} \psi_j^0(1) (-1)^{j-1} h^{2j-2} A^{j-1} \left[ A^2 w_0 - \frac{q}{2(1-v) D} \right] = 0,$$

where the values of  $\psi_j^0$  are given in (1.2). The first three terms of this equation (1.23) are

$$(1.24) \quad \left( 1 - \frac{4}{5} h^2 A + \frac{27}{175} h^4 A^2 - \dots \right) \left[ A^2 w_0 - \frac{q}{2(1-v) D} \right] = 0.$$

This equation is identical, up to the terms of the order  $h^4$ , with the equation derived in [18] directly, provided that we consider in equations (1.1) and (1.4)  $N = 2$ .

It is worth noticing that the biharmonic solution of the equations (1.22) and (1.23) corresponding to Kirchhoff's theory, represents a particular integral of these equations.

**2.** It remains to determine the boundary conditions for the differential equation (1.22). For this purpose it is necessary to substitute in the equation (1.16) for the operator  $L_1$ ,  $L_2$ ,  $L_1^{(k)}$  and  $L_2^{(k)}$  their expansions (1.17), and (1.18), and to integrate with respect to  $\zeta$ . No elementary operations and arrangements are given here, only the result is presented in the form

$$\begin{aligned}
 (2.1) \quad & \frac{9}{8h^3} \int_C \sum_{j=1}^{\infty} \sum_{k=1}^{\infty} \sum_{l=1}^{\infty} (-1)^{j+k} h^{2j+2k-6} \left\{ \frac{2-\gamma}{\gamma-1} \left[ h^2 A_{j,0,k} \Delta^j w_0 \frac{\partial \Delta^{k-1} \delta w_0}{\partial n} - \right. \right. \\
 & - h^2 A_{j,0,k} \frac{\partial \Delta^j w_0}{\partial n} \Delta^{k-1} \delta w_0 + B_{j,k} \Delta^{j-1} w_0 \frac{\partial \Delta^{k-1} \delta w_0}{\partial n} - B_{j,k} \frac{\partial \Delta^{k-1} w_0}{\partial n} \Delta^{k-1} \delta w_0 + \\
 & + h^2 C_{j,k} \Delta^j w_0 \frac{\partial \Delta^{k-1} w_0}{\partial n} - h^2 C_{j,k} \frac{\partial \Delta^j w_0}{\partial n} \Delta^{k-1} \delta w_0 + (-1)^l h^{2l+2} D_{j,k,l} \Delta^{j+l} w_0 \cdot \\
 & \cdot \frac{\partial \Delta^{k-1} \delta w_0}{\partial n} - (-1)^l h^{2l+2} D_{j,k,l} \frac{\partial \Delta^{j+l} w_0}{\partial n} \Delta^{k-1} \delta w_0 \Big] + \\
 & + 2 \left[ h^2 E_{j,0,k} \Delta^j w_0 \frac{\partial \Delta^{k-1} \delta w_0}{\partial n} - h^2 E_{j,0,k} \frac{\partial \Delta^j w_0}{\partial n} \Delta^{k-1} \delta w_0 + \right. \\
 & + (-1)^l h^{2l+2} E_{j,k,l} \Delta^{j+l} w_0 \frac{\partial \Delta^{k-1} \delta w_0}{\partial n} - (-1)^l h^{2l+2} E_{j,k,l} \frac{\partial \Delta^{j+l} w_0}{\partial n} \Delta^{k-1} \delta w_0 \Big] + \\
 & + h^4 F_{j,1,k} \frac{\partial \Delta^j w_0}{\partial n} \Delta^k \delta w_0 + (-1)^l h^{2l+2} F_{j,k,l} \Delta^{j+l} w_0 \frac{\partial \Delta^{k-1} \delta w_0}{\partial n} - \\
 & - (-1)^l h^{2l+2} F_{j,k,l} \frac{\partial \Delta^{j+l} w_0}{\partial n} \Delta^{k-1} \delta w_0 + 2 \left[ h^2 A_{j,0,k} \frac{\partial^2 \Delta^{j-1} w_0}{\partial n^2} \frac{\partial \Delta^{k-1} \delta w_0}{\partial n} + \right. \\
 & + h^2 A_{j,0,k} \left( \frac{\partial^2 \Delta^{j-1} w_0}{\partial n \partial s} - \frac{\partial \alpha}{\partial s} \frac{\partial \Delta^{j-1} w_0}{\partial s} \right) \frac{\partial \Delta^{k-1} \delta w_0}{\partial s} - h^2 A_{j,0,k} \frac{\partial \Delta^j w_0}{\partial n} \Delta^{k-1} \delta w_0 + \\
 & + (-1)^l h^{2l+2} A_{j,k,l} \Delta^{j+l} w_0 \frac{\partial \Delta^{k-1} \delta w_0}{\partial n} - (-1)^l h^{2l+2} A_{j,k,l} \frac{\partial \Delta^{j+l} w_0}{\partial n} \Delta^{k-1} \delta w_0 \Big] + \\
 & \left. + \frac{4h^4}{3\gamma D} \psi_{j+k}^0(1) \left[ \Delta^{j-1} q \frac{\partial \Delta^{k-1} \delta w_0}{\partial n} - \frac{\partial \Delta^{j-1} q}{\partial n} \Delta^{k-1} \delta w_0 \right] \right\} ds = 0,
 \end{aligned}$$

where we denote

$$\begin{aligned}
 (2.2) \quad & A_{j,k,l} = \int_0^1 \varphi_{j+k}^0 \varphi_l^0 d\zeta, \\
 & B_{j,k} = \int_0^1 \frac{d\psi_j^0}{d\zeta} \varphi_k^0 d\zeta, \\
 & C_{j,k} = \int_0^1 \left( \frac{d\psi_{j+1}^0}{d\zeta} - \varphi_j^0 \right) \frac{d\psi_{k+1}^0}{d\zeta} d\zeta,
 \end{aligned}$$

$$D_{j,k,l} = \int_0^1 \left( \frac{d\psi_{j+k+1}^0}{d\zeta} - \varphi_{j+k}^0 \right) \left( \frac{d\psi_{l+1}^0}{d\zeta} - \varphi_l^0 \right) d\zeta ,$$

$$E_{j,k,l} = \int_0^1 \frac{d\psi_{j+k+1}^0}{d\zeta} \frac{d\psi_{l+1}^0}{d\zeta} d\zeta ,$$

$$F_{j,k,l} = \int_0^1 \left( \frac{d\varphi_{j+k}^0}{d\zeta} + \psi_{j+k}^0 \right) \left( \frac{d\varphi_{l+1}^0}{d\zeta} + \psi_{l+1}^0 \right) d\zeta .$$

Some first values of the coefficients  $A_{j,k,l} - F_{j,k,l}$  are presented in Tab. 1.

Further we substitute these coefficients into (2.1) and we arrange the individual terms according to the variations  $\Delta^k \delta w_0 / \partial n$ ,  $\Delta^k \delta w_0 / \partial s$  and  $\Delta^k \delta w_0$ . In the calculations the terms containing  $\Delta^k q$  and  $\partial \Delta^k q / \partial n$  must be eliminated by using the equation (1.23). We obtain

$$(2.3) \quad \int_C \left\{ \left[ 2\gamma \left( \frac{\partial^2 w_0}{\partial n^2} + v \frac{\partial \alpha}{\partial s} \frac{\partial w_0}{\partial n} + v \frac{\partial^2 w_0}{\partial s^2} \right) - \frac{4}{5} \gamma v h^2 \left( \frac{\partial^2 \Delta w_0}{\partial s^2} + \frac{\partial \alpha}{\partial s} \frac{\partial \Delta w_0}{\partial n} \right) - \frac{4}{525} \gamma v h^4 \left( \frac{\partial^2 \Delta^2 w_0}{\partial s^2} + \frac{\partial \alpha}{\partial s} \frac{\partial \Delta^2 w_0}{\partial n} \right) - \dots \right] \frac{\partial \delta w_0}{\partial n} + \right.$$

$$+ \left[ \frac{8}{5} v h^2 \left( \frac{\partial^2 w_0}{\partial n^2} + v \frac{\partial \alpha}{\partial s} \frac{\partial w_0}{\partial n} + v \frac{\partial^2 w_0}{\partial s^2} \right) + \frac{4}{525} (\gamma + 2) h^4 \Delta^2 w_0 - \frac{h^4}{525} (85\gamma^2 - 332\gamma + 340) \left( \frac{\partial^2 \Delta w_0}{\partial s^2} + \frac{\partial \alpha}{\partial s} \frac{\partial \Delta w_0}{\partial n} \right) - \dots \right] \frac{\partial \Delta \delta w_0}{\partial n} +$$

$$+ \left[ \frac{8}{525} v h^4 \left( \frac{\partial^2 w_0}{\partial n^2} + v \frac{\partial \alpha}{\partial s} \frac{\partial w_0}{\partial n} + v \frac{\partial^2 w_0}{\partial s^2} \right) + \dots \right] \frac{\partial \Delta^2 \delta w_0}{\partial n} + \dots +$$

$$+ \left[ \gamma^2 \left( \frac{\partial^2 w_0}{\partial n \partial s} - \frac{\partial \alpha}{\partial s} \frac{\partial w_0}{\partial s} \right) + \frac{2}{5} h^2 \gamma (2 - \gamma) \left( \frac{\partial^2 \Delta w_0}{\partial n \partial s} - \frac{\partial \alpha}{\partial s} \frac{\partial \Delta w_0}{\partial s} \right) + \frac{2}{525} h^4 \gamma (2 - \gamma) \left( \frac{\partial^2 \Delta^2 w_0}{\partial n \partial s} - \frac{\partial \alpha}{\partial s} \frac{\partial \Delta^2 w_0}{\partial s} \right) + \dots \right] \frac{\partial \delta w_0}{\partial s} +$$

$$+ \left[ \frac{2}{5} h^2 \gamma (2 - \gamma) \left( \frac{\partial^2 w_0}{\partial n \partial s} - \frac{\partial \alpha}{\partial s} \frac{\partial w_0}{\partial s} \right) + \frac{h^4}{525} (85\gamma^2 - 332\gamma + 340) \cdot \left( \frac{\partial^2 \Delta w_0}{\partial n \partial s} - \frac{\partial \alpha}{\partial s} \frac{\partial \Delta w_0}{\partial s} \right) + \dots \right] \frac{\partial \Delta \delta w_0}{\partial s} +$$

$$+ \left[ \frac{2}{525} \gamma (2 - \gamma) h^4 \left( \frac{\partial^2 w_0}{\partial n \partial s} - \frac{\partial \alpha}{\partial s} \frac{\partial w_0}{\partial s} \right) + \dots \right] \frac{\partial \Delta^2 \delta w_0}{\partial s} + \dots +$$

$$+ \left[ -2\gamma \frac{\partial \Delta w_0}{\partial n} \right] \delta w_0 + \left[ \frac{4}{5} h^2 (\gamma + 2) \frac{\partial \Delta w_0}{\partial n} + h^4 \frac{4(2 - \gamma)}{525} \frac{\partial \Delta^2 w_0}{\partial n} + \dots \right] \Delta \delta w_0 +$$

$$\left. + \left[ \frac{4}{525} h^4 (\gamma + 2) \frac{\partial \Delta w_0}{\partial n} + \dots \right] \Delta^2 \delta w_0 + \dots \right\} ds = 0 .$$

Table 1

$A_{1,0,1} = \frac{1}{3}\gamma^2, \quad A_{1,1,1} = A_{2,0,1} = A_{1,0,2} = \frac{2\gamma}{15}(\gamma - 2),$
$A_{1,1,2} = A_{2,0,2} = \frac{1}{1575}(85\gamma^2 - 332\gamma + 340), \quad A_{1,2,1} = A_{2,1,1} = A_{3,0,1} =$
$= A_{1,0,3} = \frac{2\gamma}{1575}(2 - \gamma),$
$B_{1,k} = 0, \quad B_{2,1} = \frac{1}{3}\gamma(2 - \gamma), \quad B_{3,1} = -\frac{2}{15}\gamma^2, \quad B_{2,2} = -\frac{2}{15}(2 - \gamma)^2,$
$B_{4,1} = \frac{2\gamma^2}{1575}, \quad B_{3,2} = \frac{1}{1575}(8 + 170\gamma - 85\gamma^2), \quad B_{2,3} = \frac{2}{1575}(\gamma - 2)^2,$
$C_{1,1} = \frac{2}{3}(\gamma - 1)(\gamma - 2), \quad C_{2,1} = \frac{4}{15}(\gamma - 1)(\gamma - 2), \quad C_{1,2} = \frac{4}{15}\gamma(\gamma - 1),$
$C_{3,1} = \frac{4}{1575}(\gamma - 1)(2 - \gamma), \quad C_{2,2} = \frac{2}{1575}(\gamma - 1)(85\gamma - 4), \quad C_{1,3} = \frac{4\gamma}{1575}(1 - \gamma),$
$D_{1,1,1} = \frac{8}{15}(\gamma - 1)^2, \quad D_{2,1,1} = D_{1,2,1} = -\frac{8}{1575}(\gamma - 1)^2, \quad D_{1,1,2} = \frac{68}{315}(\gamma - 1)^2,$
$E_{1,0,1} = \frac{1}{3}(\gamma - 2)^2, \quad E_{2,0,1} = E_{1,0,2} = E_{1,1,1} = \frac{2}{15}\gamma(\gamma - 2),$
$E_{3,0,1} = E_{1,0,3} = E_{1,2,1} = E_{2,1,1} = \frac{2\gamma}{1575}(2 - \gamma), \quad E_{1,1,2} = E_{2,0,2} =$
$= \frac{1}{1575}(85\gamma^2 - 8\gamma + 16),$
$F_{1,1,1} = F_{2,0,1} = \frac{32}{15}, \quad F_{2,1,1} = F_{1,1,2} = F_{1,2,1} = -\frac{32}{1575},$
$G_{2,1} = \frac{4}{3}\gamma, \quad G_{3,1} = 0, \quad G_{2,2} = \frac{8}{15}(\gamma + 2), \quad G_{3,2} = \frac{8}{1575}(\gamma - 2),$
$G_{2,3} = -\frac{8}{1575}(\gamma + 2).$

Let us show further that it is possible to give a physical interpretation to the terms in the brackets. We shall, therefore, introduce polymoments and shearing polyforces in the following manner: The expression

$$(2.4) \quad M_x^k = - \frac{h^2}{\gamma} \int_{-1}^1 \sigma_x \varphi_{k+1}^0 d\zeta$$

will be called the  $k$ -th bending polymoment.

Similarly the  $k$ -th twisting polymoment will be

$$(2.5) \quad M_{xy}^k = - \frac{h^2}{\gamma} \int_{-1}^1 \tau_{xy} \varphi_{k+1}^0 d\zeta$$

and the  $k$ -th shearing polyforce will be

$$(2.6) \quad Q_x^k = \frac{h}{\gamma} \int_{-1}^1 \tau_{xz} \psi_{k+1}^0 d\zeta .$$

In these relations  $\sigma_x$ ,  $\tau_{xy}$  and  $\tau_{xz}$  are normal and tangential stresses acting in the cross-section  $x = \text{const}$ .

When for the stresses we substitute the corresponding terms from Hooke's law, we obtain

$$(2.7) \quad \begin{aligned} M_x^k &= - \frac{2h^2}{\gamma} \frac{4\mu h^3}{3} \int_0^1 \left[ \frac{2-\gamma}{\gamma-1} \left( \Delta L_1 w_0 + \frac{\partial L_2 w_0}{h \partial \zeta} \right) + 2L_1 \frac{\partial^2 w_0}{\partial x^2} \right] \varphi_{k+1}^0 d\zeta = \\ &= - \frac{2\mu h^3}{\gamma} \sum_{i=1}^{\infty} (-1)^{i-1} h^{2i-2} \left[ 2A_{i,0,k+1} \frac{\partial^2 \Delta^{i-1} w_0}{\partial x^2} + \right. \\ &\quad \left. + \frac{2-\gamma}{\gamma-1} (A_{i,0,k+1} - B_{i+1,k+1}) \Delta^i w_0 \right], \end{aligned}$$

$$(2.8) \quad \begin{aligned} M_{xy}^k &= - \frac{2h^2}{\gamma} \frac{8\mu h^3}{3} \int_0^1 \frac{\partial^2 L_1 w_0}{\partial x \partial y} \cdot \varphi_{k+1}^0 d\zeta = \\ &= - \frac{4\mu h^3}{\gamma} \sum_{i=1}^{\infty} (-1)^{i-1} h^{2i-2} A_{i,0,k+1} \frac{\partial^2 \Delta^{i-1} w_0}{\partial x \partial y}, \end{aligned}$$

$$(2.9) \quad \begin{aligned} Q_x^k &= \frac{2h}{\gamma} \frac{4\mu h^3}{3} \int_0^1 \frac{\partial}{\partial x} \left( L_2 + \frac{\partial L_1}{h \partial \zeta} \right) w_0 \cdot \psi_{k+1}^0 d\zeta = \\ &= - \frac{2\mu h^3}{\gamma} \sum_{i=1}^{\infty} (-1)^{i-1} h^{2i-2} G_{i+1,k+1} \frac{\partial \Delta^i w_0}{\partial x}, \end{aligned}$$

where the values

$$(2.10) \quad G_{i,k} = \int_0^1 \left( \frac{d\varphi_i^0}{d\zeta} + \psi_i^0 \right) \psi_k^0 d\zeta$$

are also given in table 1.

When we consider that on the edge (Fig. 1) it holds [19]

$$(2.11) \quad \begin{aligned} \frac{\partial w_0}{\partial t} &= \frac{\partial w_0}{\partial s}, \\ \frac{\partial^2 w_0}{\partial n \partial t} &= \frac{\partial^2 w_0}{\partial n \partial s} - \frac{\partial \alpha}{\partial s} \frac{\partial w_0}{\partial s} \end{aligned}$$

and the operator  $\Delta$  is given by the expression (1.19), then we can determine the values  $M_n^k$ ,  $M_{ns}^k$ ,  $Q_n^k$  on the edge by a transformation of the moments and the shearing forces given in rectangular coordinates. We shall give here the three first polymoments and shearing forces up to the order  $h^4$  only

$$(2.12) \quad \begin{aligned} M_n^0 &= -\frac{8}{3} \mu h^3 \left[ \frac{\partial^2 w_0}{\partial n^2} + v \frac{\partial \alpha}{\partial s} \frac{\partial w_0}{\partial n} + v \frac{\partial^2 w_0}{\partial s^2} - \frac{2}{5} vh^2 \left( \frac{\partial^2 \Delta w_0}{\partial s^2} + \frac{\partial \alpha}{\partial s} \frac{\partial \Delta w_0}{\partial n} \right) - \right. \\ &\quad \left. - \frac{2}{525} vh^4 \left( \frac{\partial^2 \Delta^2 w_0}{\partial s^2} + \frac{\partial \alpha}{\partial s} \frac{\partial \Delta^2 w_0}{\partial n} \right) - \dots \right], \\ M_n^1 &= \frac{4\mu h^3}{3\gamma} \left[ \frac{8}{5} v \left( \frac{\partial^2 w_0}{\partial n^2} + v \frac{\partial \alpha}{\partial s} \frac{\partial w_0}{\partial n} + v \frac{\partial^2 w_0}{\partial s^2} \right) + \frac{4}{525} (\gamma + 2) h^2 \Delta^2 w_0 - \right. \\ &\quad \left. - \frac{h^2}{525} (85\gamma^2 - 332\gamma + 340) \left( \frac{\partial^2 \Delta w_0}{\partial s^2} + \frac{\partial \alpha}{\partial s} \frac{\partial \Delta w_0}{\partial n} \right) - \dots \right], \\ M_n^2 &= -\frac{32}{1575} v \frac{\mu h^3}{\gamma} \left[ \frac{\partial^2 w_0}{\partial n^2} + v \frac{\partial \alpha}{\partial s} \frac{\partial w_0}{\partial n} + v \frac{\partial^2 w_0}{\partial s^2} + \dots \right], \\ M_{ns}^0 &= -\frac{4}{3} \mu h^3 \left[ \gamma \left( \frac{\partial^2 w_0}{\partial n \partial s} - \frac{\partial \alpha}{\partial s} \frac{\partial w_0}{\partial s} \right) + \frac{2}{5} (2 - \gamma) h^2 \left( \frac{\partial^2 \Delta w_0}{\partial n \partial s} - \frac{\partial \alpha}{\partial s} \frac{\partial \Delta w_0}{\partial s} \right) + \right. \\ &\quad \left. + \frac{2}{525} (2 - \gamma) h^4 \left( \frac{\partial^2 \Delta^2 w_0}{\partial n \partial s} - \frac{\partial \alpha}{\partial s} \frac{\partial \Delta^2 w_0}{\partial s} \right) + \dots \right], \\ M_{ns}^1 &= \frac{4\mu h^3}{3\gamma} \left[ \frac{2}{5} \gamma(\gamma - 2) \left( \frac{\partial^2 w_0}{\partial n \partial s} - \frac{\partial \alpha}{\partial s} \frac{\partial w_0}{\partial s} \right) + \frac{h^2}{525} (85\gamma^2 - 332\gamma + 340) \cdot \right. \\ &\quad \left. \cdot \left( \frac{\partial^2 \Delta w_0}{\partial n \partial s} - \frac{\partial \alpha}{\partial s} \frac{\partial \Delta w_0}{\partial s} \right) + \dots \right], \\ M_{ns}^2 &= -\frac{4\mu h^3}{3\gamma} \left[ \frac{2}{525} \gamma(\gamma - 2) \left( \frac{\partial^2 w_0}{\partial n \partial s} - \frac{\partial \alpha}{\partial s} \frac{\partial w_0}{\partial s} \right) + \dots \right], \end{aligned}$$

(2.14)

$$\begin{aligned} Q_n^0 &= -\frac{8}{3} \mu h^3 \frac{\partial \Delta w_0}{\partial n}, \\ Q_n^1 &= -\frac{4\mu h^3}{3\gamma} \left[ \frac{4}{5}(\gamma + 2) \frac{\partial \Delta w_0}{\partial n} - \frac{4}{525}(\gamma - 2) h^2 \frac{\partial \Delta^2 w_0}{\partial n} + \dots \right], \\ Q_n^2 &= -\frac{4\mu h^3}{3\gamma} \left[ \frac{4}{525}(\gamma + 2) \frac{\partial \Delta w_0}{\partial n} + \dots \right]. \end{aligned}$$

When comparing the expressions in the brackets of the equation (2.3) to the equations of the above polymoments and polyforces (2.12) to (2.14), we find that equation (2.3) can be written in the compact form

$$(2.15) \quad \begin{aligned} &\frac{3\gamma}{4\mu h^3} \int_C \left( -M_n^0 \frac{\partial \delta w_0}{\partial n} + h^2 M_n^1 \frac{\partial \Delta \delta w_0}{\partial n} - h^4 M_n^2 \frac{\partial \Delta^2 \delta w_0}{\partial n} + \dots - \right. \\ &- M_{ns}^0 \frac{\partial \delta w_0}{\partial s} + h^2 M_{ns}^1 \frac{\partial \Delta \delta w_0}{\partial s} - h^4 M_{ns}^2 \frac{\partial \Delta^2 \delta w_0}{\partial s} + \dots + \\ &\left. + Q_n^0 \delta w_0 - h^2 Q_n^1 \Delta \delta w_0 + h^4 Q_n^2 \Delta^2 \delta w_0 - \dots \right) ds = 0. \end{aligned}$$

Equation (2.15) can be arranged into the form

$$(2.16) \quad \int_C \sum_{i=0}^{\infty} (-1)^{i+1} h^{2i} \left[ M_n^i \frac{\partial \Delta^i \delta w_0}{\partial n} - \left( Q_n^i + \frac{\partial M_{ns}^i}{\partial s} \right) \Delta^i \delta w_0 \right] ds = 0.$$

From this equation we obtain the static boundary conditions in the form representing a generalization of Kirchhoff's conditions

$$(2.17) \quad M_n^i = 0, \quad Q_n^i + \frac{\partial M_{ns}^i}{\partial s} = 0, \quad (i = 0, 1, 2, \dots).$$

We can see that apart from fulfilling the ordinary boundary conditions of Kirchhoff, which formally correspond to the case  $i = 0$ , (of course when neglecting the terms of order  $h^2$  and higher in the equations (2.12 to 2.14)) it is required that all, the  $i$ -th bending polymoments and the  $i$ -th generalized shearing polyforces, should be equal to zero at the edge. It is obvious that the introduction of one function  $w_0(x, y)$  enables to satisfy for all  $|\zeta| \leq 1$  two boundary conditions only and, therefore, on the free edge there remain the nonvanishing stresses  $\tau_{nz}$  and  $\tau_{ns}$ . These will represent the boundary effects of the Saint-Venant type and thus the solution corresponds to the fundamental state of stress [20]. However, the above solution is more general than that corresponding to the biharmonic solution only.

### References

- [1] *I. Babuška, M. Práger*: Reissnerian Algorithms in the Theory of Elasticity. Bulletin de l'Académie Polonaise des Sciences, Série des sciences techniques, Vol. VIII, No. 8, 411–417, 1960, (in Russian) Механика, сб. переводов, Но 6, стр. 123—128, 1961.
- [2] *I. Babuška et al.*: Algorithmi of the Reissnerian Type in the Mathematical Theory of Elasticity (in Czech), Sborník 24 Fak. inž. stav. ČVUT v Praze, Státní ped. naklad., pp. 15–47, Praha 1961.
- [3] *I. Babuška*: Die Stabilität mit Rücksicht auf das Definitionsgebiet und die Frage der Formulierung des Plattenproblems (Vorbericht), Aplikace Matematiky, 7, No 6, str. 457–461, 1962, (in Russian) Механика, сб. переводов, Но 2, стр. 149—153, 1963.
- [4] *I. Babuška*: Problems of Optimal Reduction of Three-Dimensional Problems of the Theory of Elasticity. Theory of Plates and Shells, pp. 15–28, Vydatelstvo SAV, Bratislava, 1966.
- [5] *A. И. Лурье*: К теории толстых плит. Прикладная математика и механика, Т. VI, Вып. 2–3, стр. 151—168, 1942.
- [6] *A. И. Лурье*: Пространственные задачи теории упругости. Гос. изд. техн.-теор. лит., Москва, 1955.
- [7] *A. Л. Гольденвейзер*: Построение приближенной теории изгиба пластиинки методом асимптотического интегрирования уравнений теории упругости. Прикл. мат. и мех. Т. XXVI, Но. 4, стр. 668—686, 1962.
- [8] *K. O. Friedrichs, R. F. Dressler*: A Boundary-Layer Theory for Elastic Plates. Communications on Pure and Applied Mathematics, Vol. XIV, pp. 1–33, 1961.
- [9] *И. И. Ворович*: Некоторые математические вопросы теории пластин и оболочек. Механика твердого тела. Труды всесоюзного съезда по теоретической и прикладной механике, стр. 116—136, Изд. Наука, Москва 1966.
- [10] *И. И. Ворович*: Общие проблемы теории пластин и оболочек. Всесоюзная конф. по теории оболочек и пластинок 1966, стр. 896—903, Изд. Наука, Москва, 1966.
- [11] *A. L. Goldenveizer*: The principles of reducing three-dimensional problems of elasticity to two-dimensional problems of the theory of plates and shells. Applied Mechanics, Proc. of the 11th Int. Congr. of Appl. Mech., Munich (Germany) 1964, Ed. H. Görtler, pp. 306—311, Springer Verlag, Berlin — Heidelberg — New York, 1966.
- [12] *E. Reissner*: On the foundation of the theory of elastic shells. Applied Mechanics, Proc. of the 11th Int. Congr. of Appl. Mech., Munich (Germany) 1964, Ed. H. Görtler, pp. 20—30, Springer Verlag, Berlin — Heidelberg — New York, 1966.
- [13] *L. N. G. Filon*: On the expansion of polynomials in series of functions. Proc. London Math. Soc., Vol. 4, II series, pp. 396—430, 1906.
- [14] *L. H. Donnell*: A theory for thick plates, Proc. 2nd U.S. Nat. Congr. Appl. Mech., pp. 369 to 373, 1954.
- [15] *В. А. Агарев*: Метод начальных функций для двухмерных краевых задач теории упругости. Изд. АН УССР, Киев, 1963.
- [16] *Л. С. Лейбензон*: Собрание трудов, Т. 1, Изд. АН СССР, Москва 1951.
- [17] *В. К. Прокопов*: Применение символического метода к выводу уравнений теории плит. Прикл. мат. и мех., Т 29, Вып. 5, стр. 902—919, 1965.
- [18] *A. Hanuška*: The second approximation of the Reissnerian algorithmus in the theory of bending of plates (in Slovak), Stavebnicky časopis SAV, XV, 9, pp. 523—540, 1967.
- [19] *E. H. Mansfield*: The bending and stretching of plates (Int. Series of Monographs on Aeronautics and Astronautics. Div. I, vol. 6, Pergamon Press, Oxford — London — New York, 1964.
- [20] *E. Reissner*: On the derivation of boundary conditions for plate theory. Proc. Roy. Soc., London (A) 276, pp. 178—186, 1963.

## Súhrn

# REISSNEROVSKÉ ALGORITMY V SPRESNENÝCH TEÓRIACH OHYBU DOSÁK

ALEXANDER HANUŠKA

V článku sa vychádza z teórie Reissnerovských algoritmov, predložených I. Babuškom a M. Prágerom. Pre špeciálny prípad jednej neznámej funkcie  $w_0(x, y)$  sú vyjadrené posuny  $u, v, w$  pomocou diferenciálnych operátorov nekonečného rádu rovnicami (1.5). Pri aplikácii Lagrangeovho princípu je treba použiť zobecnené Greenove formuly (1.12) odvodené V. K. Prokopovom. Použitím týchto formúl a integrovaním podľa  $\zeta$  obdrží sa diferenciálna rovnica nekonečného rádu (1.22). Je ukázané ďalej, že príslušným okrajovým podmienkam je možné dať fyzikálnu interpretáciu zavedením polymomentov a polysíl podľa (2.4–2.6). Obdržané okrajové podmienky (2.17) predstavujú zobecnenie Kirchhoffových okrajových podmienok a tedy uvažovaný prípad jednej funkcie  $w_0$  zodpovedá len základnému stavu napäťosti.

## Резюме

# РЕЙСНЕРОВСКИЕ АЛГОРИФМЫ В УТОЧНЕННЫХ ТЕОРИЯХ ИЗГИБА ПЛАСТИНОК

АЛЕКСАНДЕР ГАНУШКА (ALEXANDER HANUŠKA)

Статья исходит из теории Рейснеровских алгорифмов, предложенных И. Бабушком и М. Прагером. Для специального случая одной неизвестной функции  $w_0(x, y)$  выражаются перемещения  $u, v, w$  при помощи дифференциальных операторов бесконечного порядка уравнениями (1.5). При применении принципа Лагранжа надо пользоваться обобщенными формулами Грина (1.12) выведенными В. К. Прокоповым. Использованием этих формул и интегрированием по  $\zeta$  получено дифференциальное уравнение бесконечного порядка (1.22). В дальнейшем показано, что соответствующие граничные условия можно интерпретировать посредством введения полимоментов и полисил следуя уравнениям (2.4–2.6). Полученные граничные условия (2.17) представляют обобщение граничных условий Кирхгофа и рассматриваемый случай одной функции соответствует только основному состоянию напряжения.

*Author's address:* Ing. Alexander Hanuška CS.c, Ústav stavebnictva a architektúry SAV, Dúbravská cesta 4, P.O.B. 1191, Bratislava.